

**DRAPER**

# **A Transistor-less, Wireless Neural Stimulator**

Daniel Freeman

5/3/2016

# Problem Statement

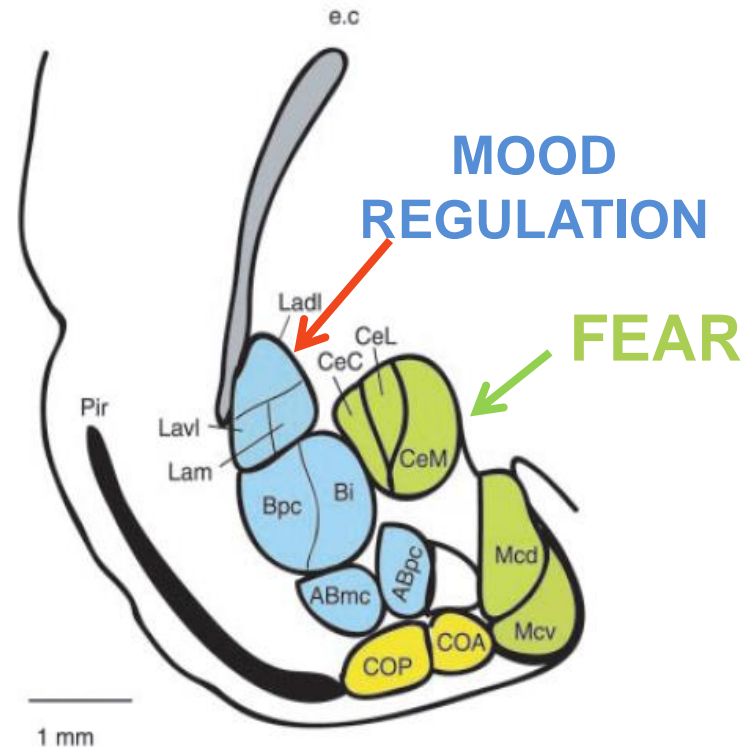
**Problem:** Tethered implants exhibit scar tissue growth, reducing control over the spatial pattern of neural excitation



## Amygdaloid Complex

**Basolateral Group (blue):** Project to prefrontal cortex

**Centromedial Group (green):** Project to hypothalamus and brainstem



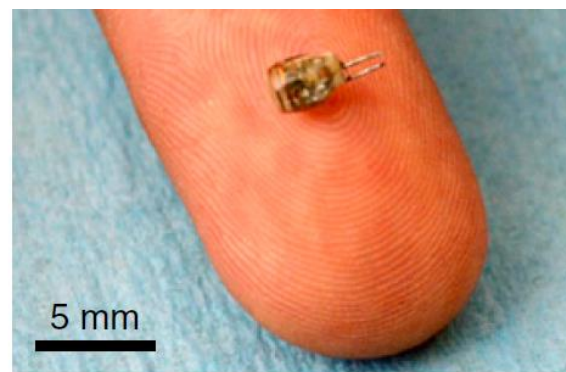
# Wireless Neural Stimulators

- **Solution**: Untethered stimulators show less scar tissue growth
- **Problem**: Wireless energy transfer is difficult for sub-millimeter implants

*RF BION*



*Mid-Field Powering*



*Microwave Powered*



*FLAMES Stimulator*

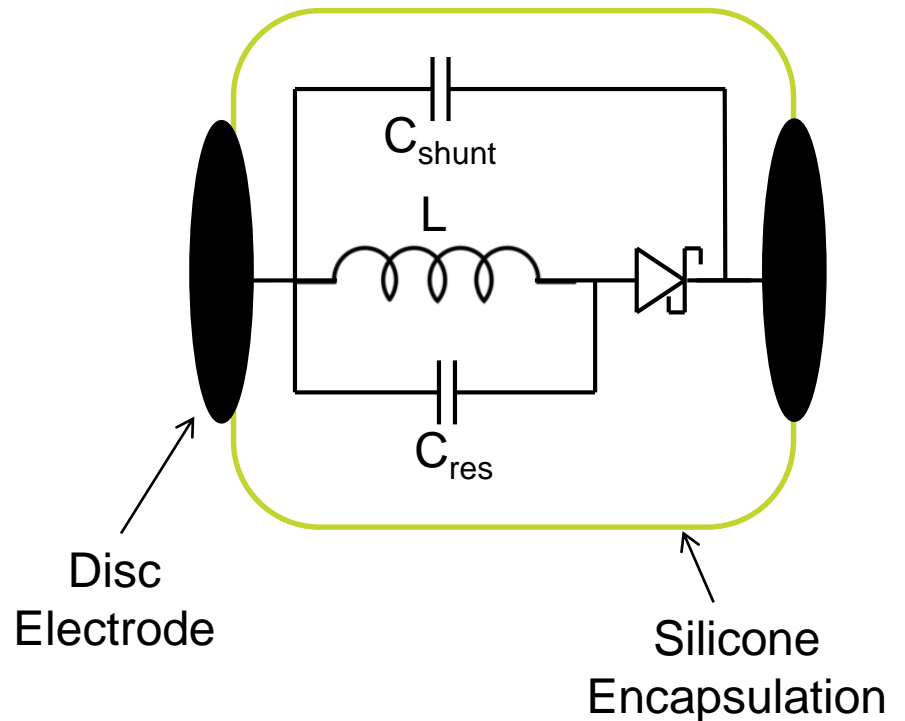


# A Transistor-less Neural Stimulator

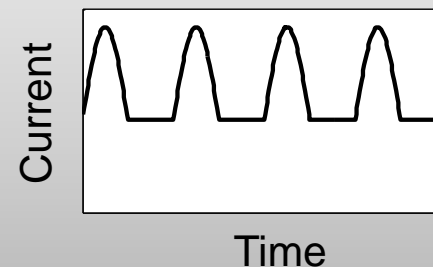
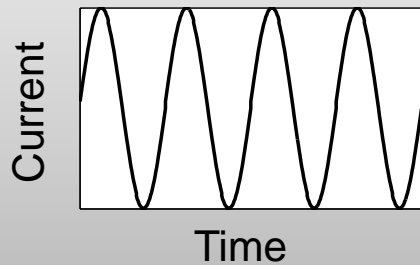
Size of implant is determined by receive antenna for power



Size can be reduced by removing the voltage requirements associated with transistors

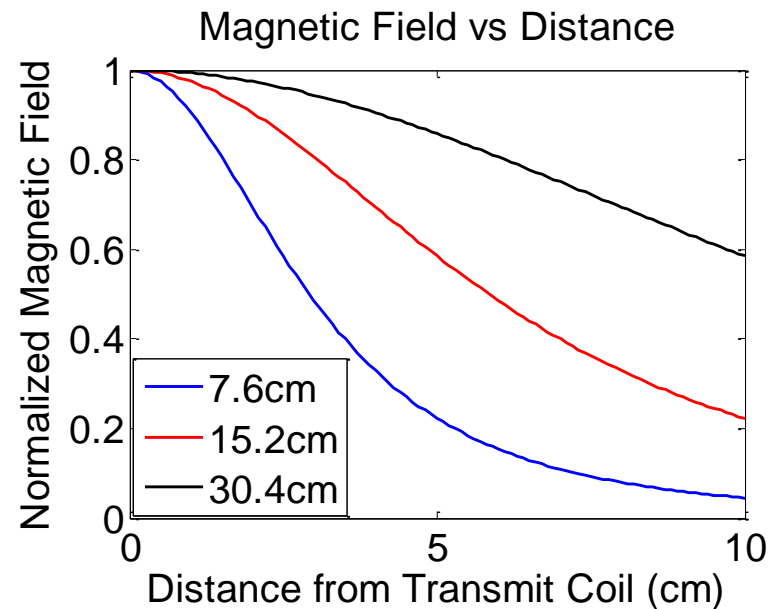
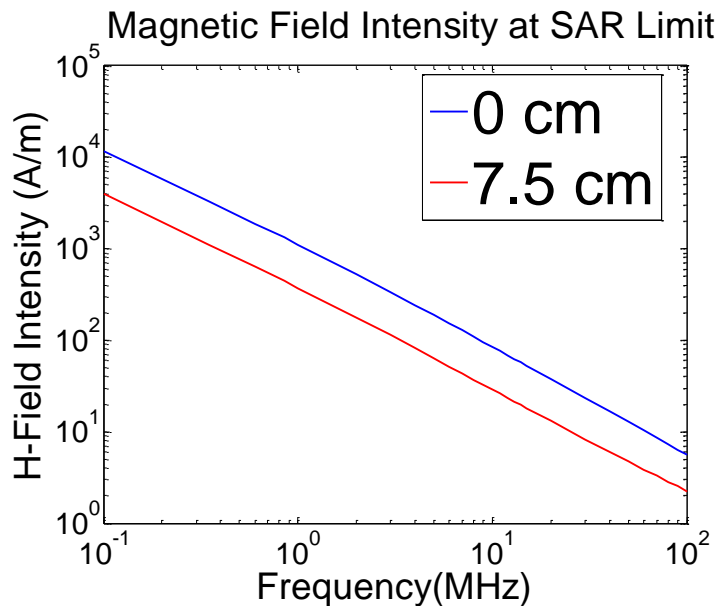
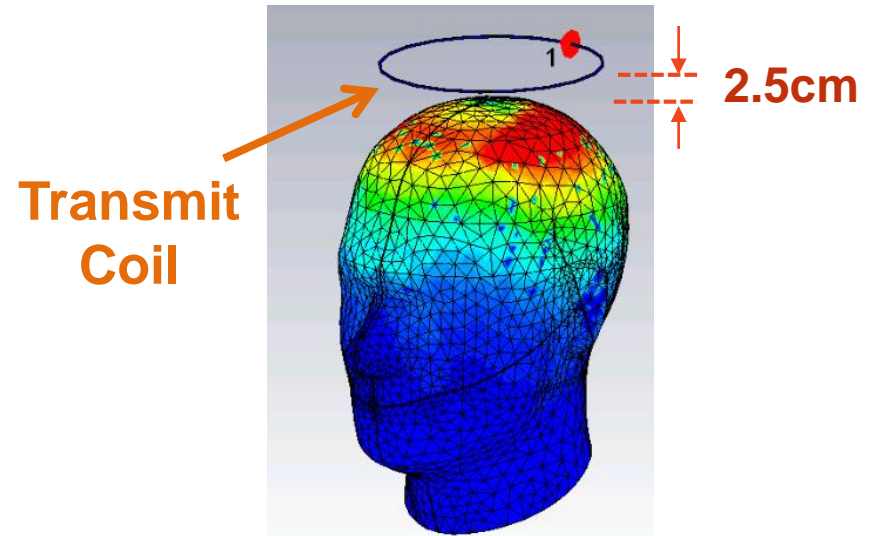


*Rectification with Diode Produces DC*



# Estimating the Magnetic Field Intensity in the Body

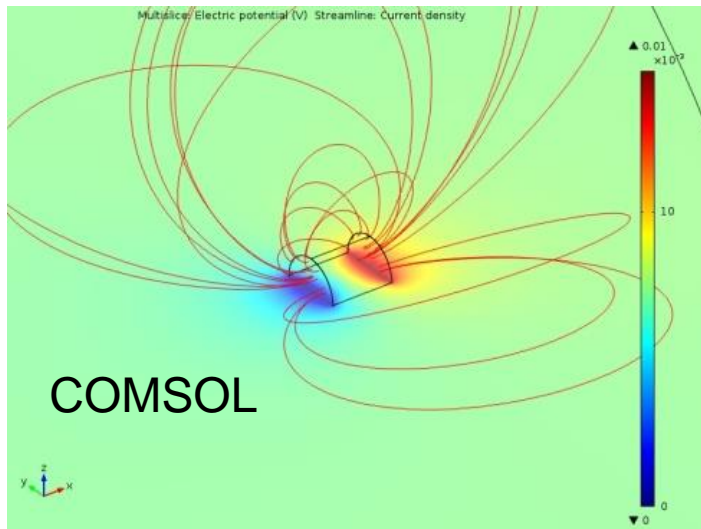
- Maximum allowed magnetic field set by FCC
- SAR Limit estimates the amount of heating in the body



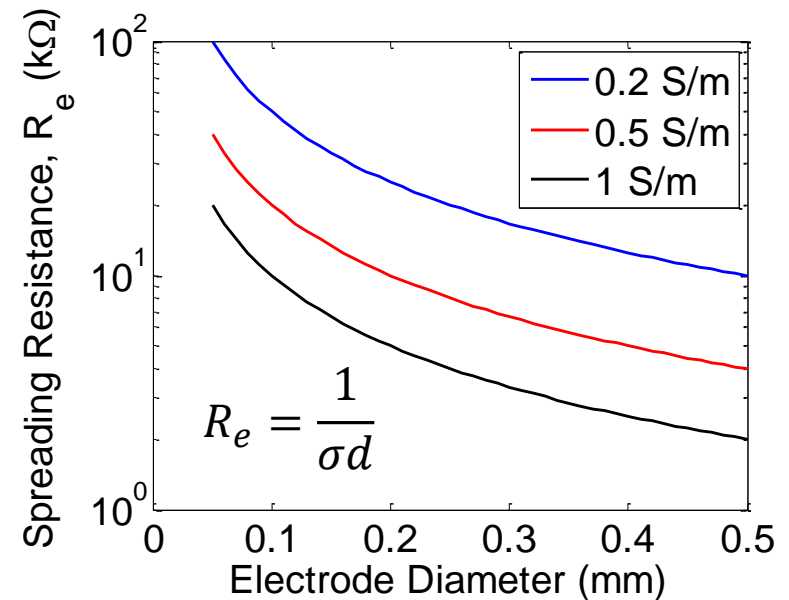
# Estimating the Load Impedance

- Total load for electrodes of 300 - 500 $\mu\text{m}$  and a conductivity of 0.5 S/m = **10k $\Omega$**
- To reach a threshold current of 25 $\mu\text{A}$ , we need 250mV across the load

## Computational Estimates



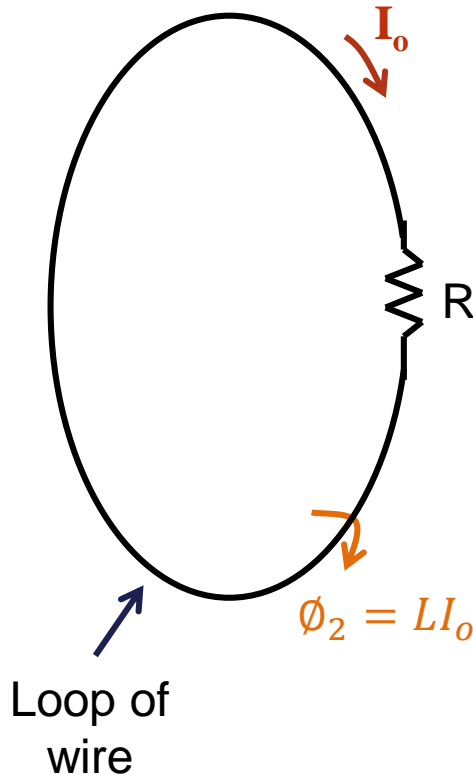
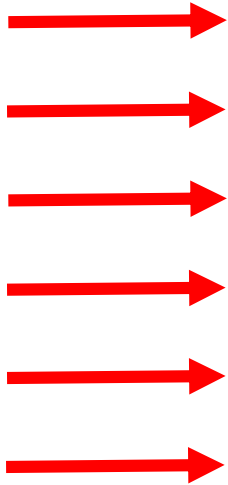
## Analytical Estimates



# Estimate Current and Power Delivered to Load

Applied Magnetic Field

$$\Phi_1 = \mu_0 H_0 A$$



**Faraday's Law**

$$\oint E \cdot dl = - \int \frac{\partial B}{\partial t} \cdot dA$$



**Flux Rule**

$$\varepsilon = - \frac{d\Phi_{total}}{dt}$$



$$\varepsilon = - \frac{d(\Phi_1)}{dt} + \frac{d(\Phi_2)}{dt} = -I_0 R$$

**Laplace Domain**



**Power**

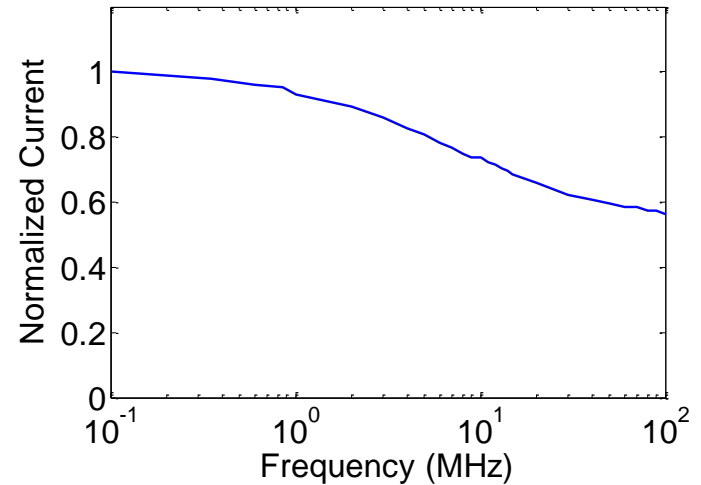
$$P(s) = \varepsilon(s)I_0(s) = \frac{(s\mu_0 H_0 A)^2 R}{(sL + R)^2}$$

**Current**

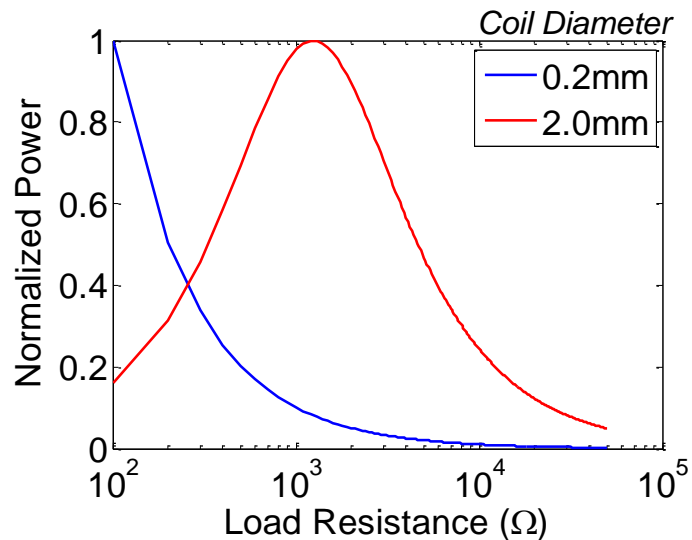
$$I_0(s) = \frac{s\mu_0 H_0 A}{sL + R}$$

# Estimate Optimal Load and Optimal Frequency

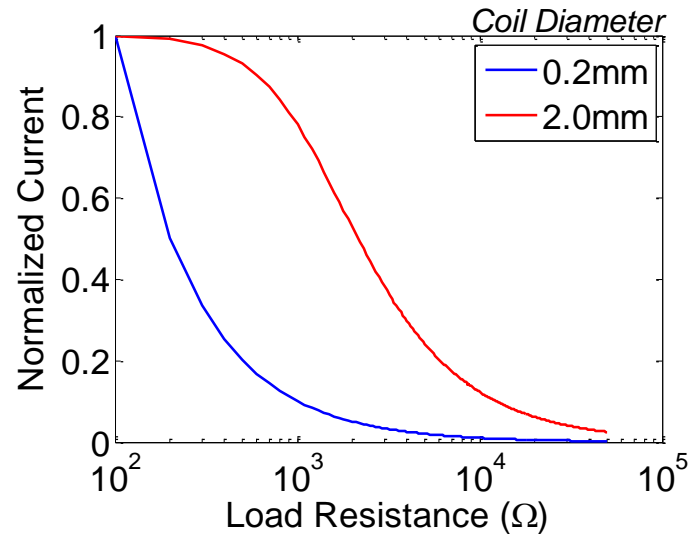
- **Optimal Load**: Make load as small as possible to maximize current
- **Optimal Frequency**: Slight improvement at lower frequencies



## Power



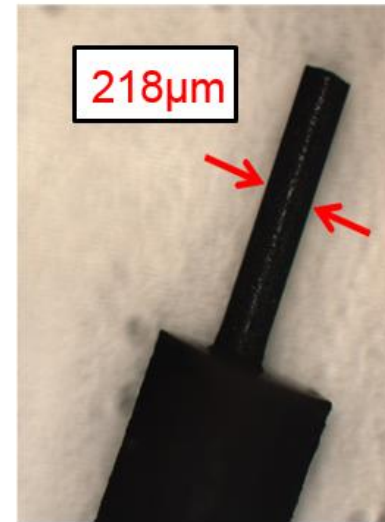
## Current



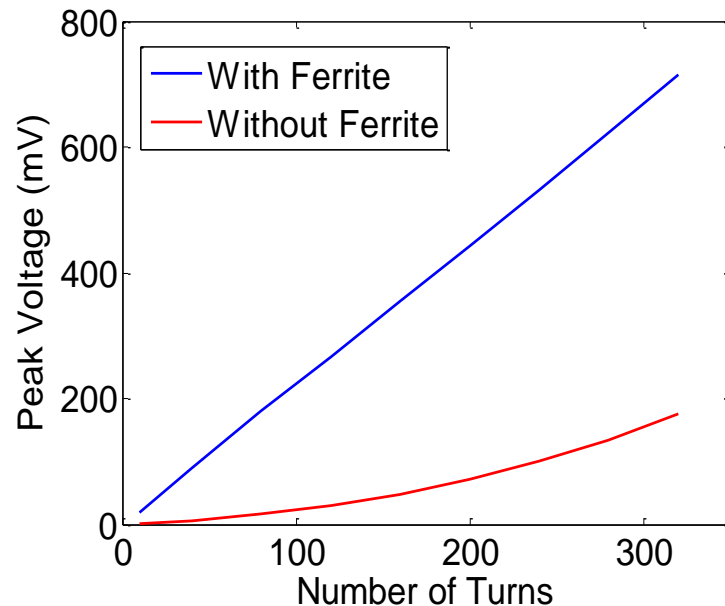


# Effect of the Ferrite Core

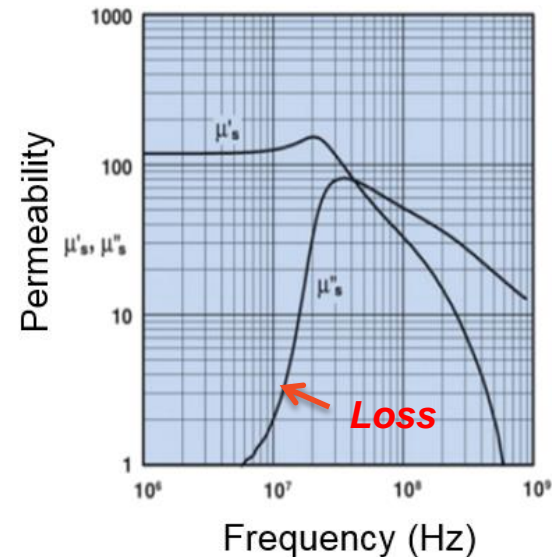
- FEM Model suggests a ferrite core is critical to achieve desired current
- **Problem**: Manufacturers do not make ferrite cores of  $< 0.5\text{mm}$  diameter
- **Solution**: We shaved down the cores to  $0.2\text{mm}$  with a diamond-tipped grinder



Effect of Ferrite Core

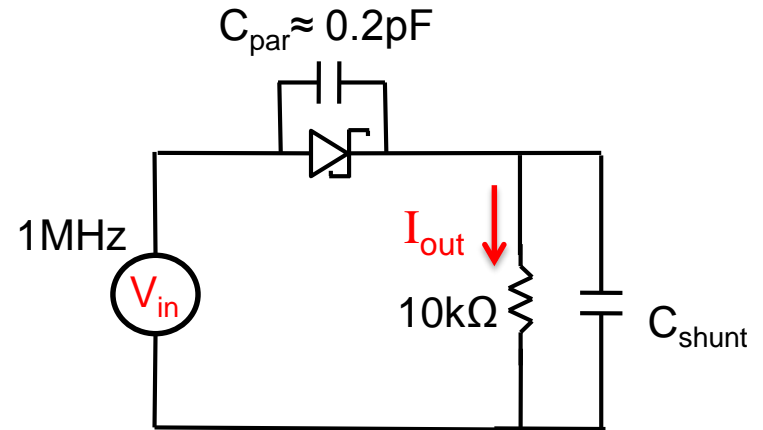


# 61 Nickel Zinc Ferrite

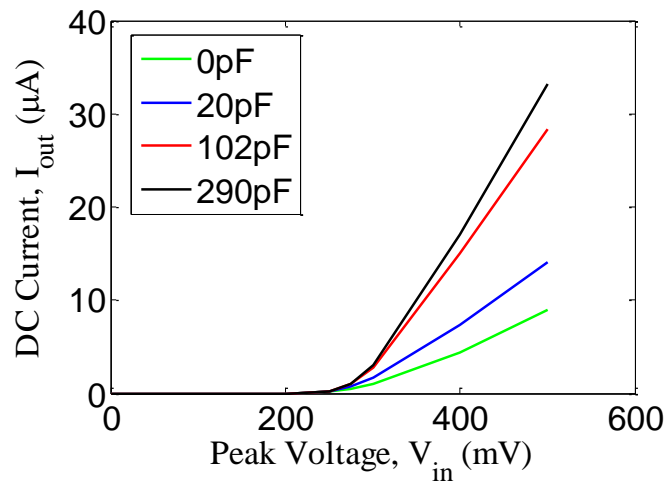


# Rectification with the Diode

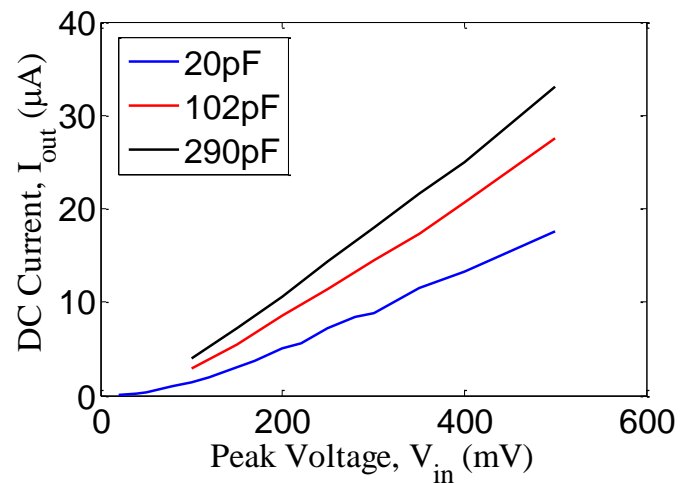
- Rectification achieved with an RF Schottky diode
- A shunt capacitor is used to facilitate rectification by compensating for parasitic capacitance ( $C_{par}$ )



Simulations (SPICE)

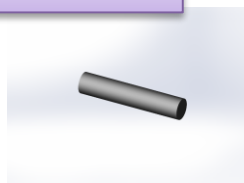


Measurements



# Process Flow for Assembly

## Components



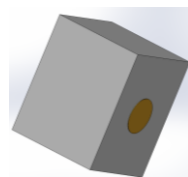
(x1)

Ferrite rod  
(200  $\mu$ m x 1mm)



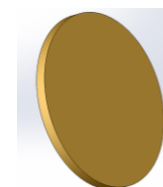
(x2)

Capacitor (250  $\mu$ m  
x 200  $\mu$ m x 250  $\mu$ m)



(x1)

Skyworks diode (250  $\mu$ m x  
200  $\mu$ m x 250  $\mu$ m)



(x2)

Roughened Pt electrode  
(300  $\mu$ m x 18  $\mu$ m)

## Assembly

1



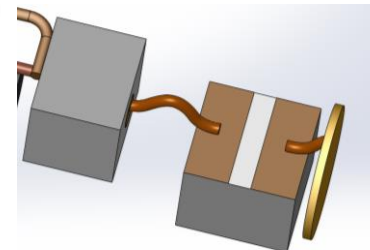
Wind the Coil

2



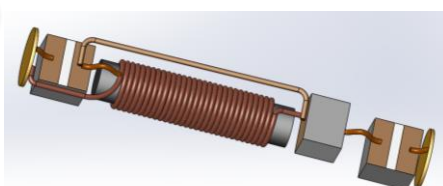
Connect resonant  
cap to electrode

3



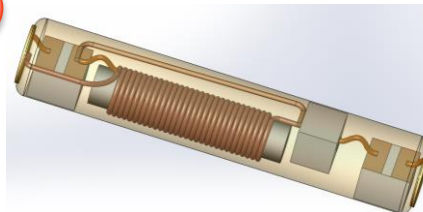
Connect diode, shunt  
cap, and Pt electrode

4



Connect coil to two  
assembled pieces

5

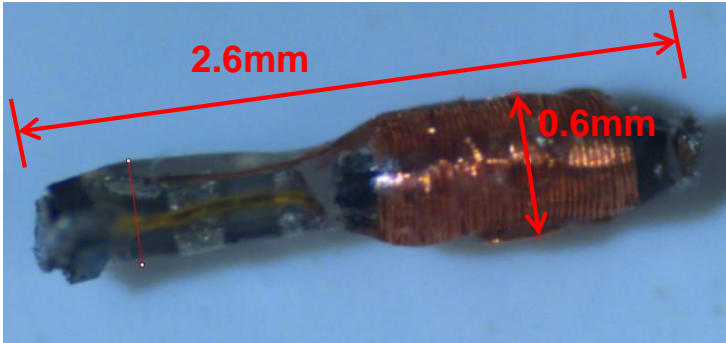


Encapsulate in silicone

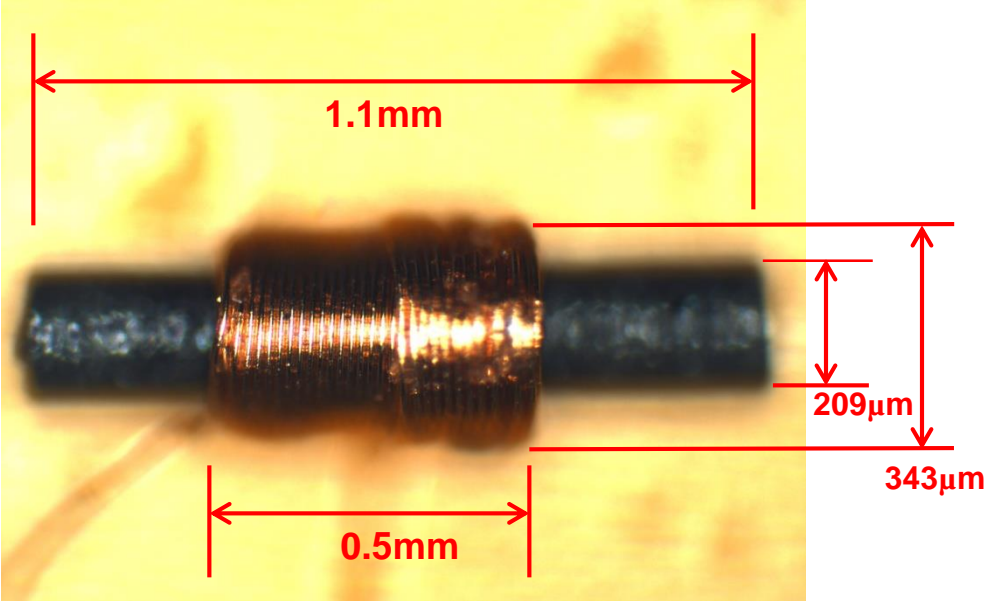
# Built Prototypes

- Prototypes assembled by hand
- Solder past and 1-mil gold wires used for interconnects
- Volume achieved:  $0.5 \text{ mm}^3$

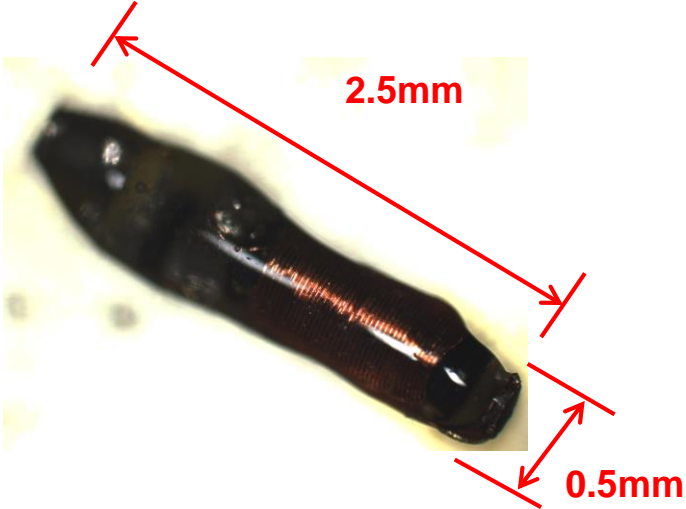
### Prototype with 0402 Caps



### Coil and Ferrite (100-turns)

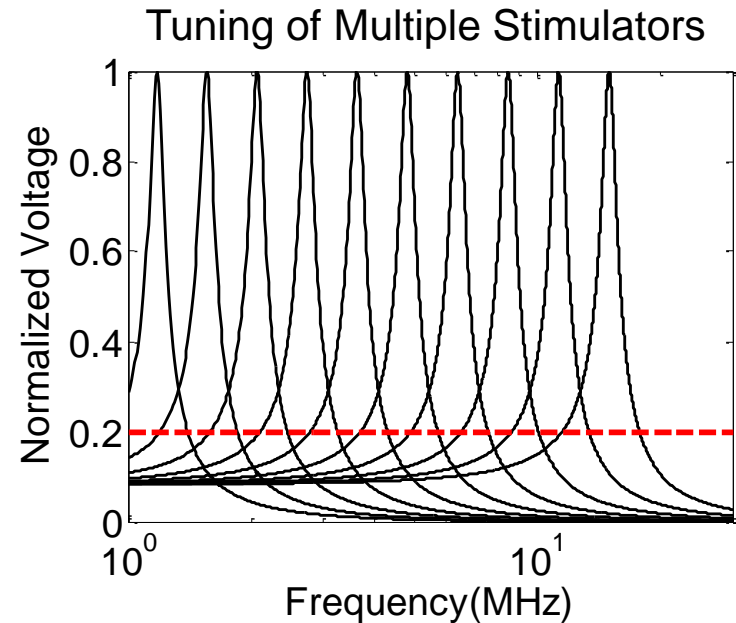
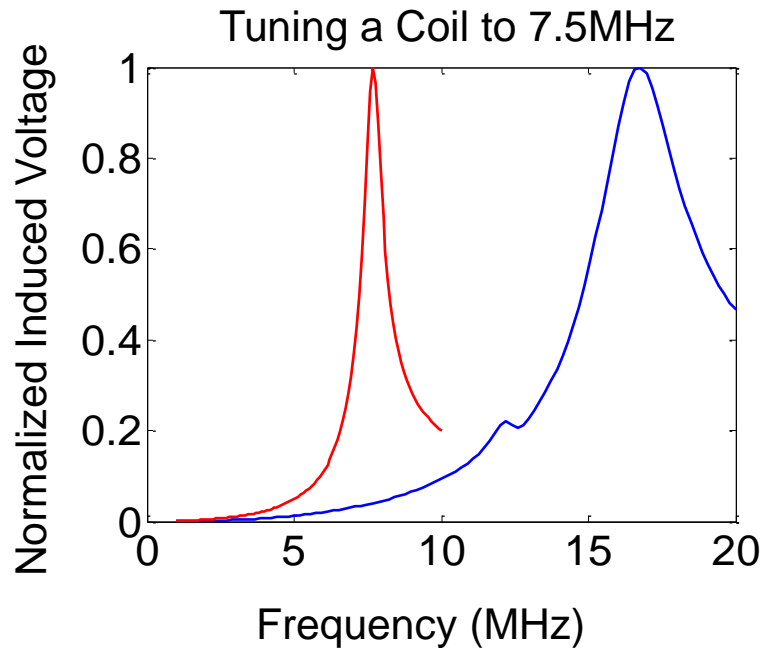
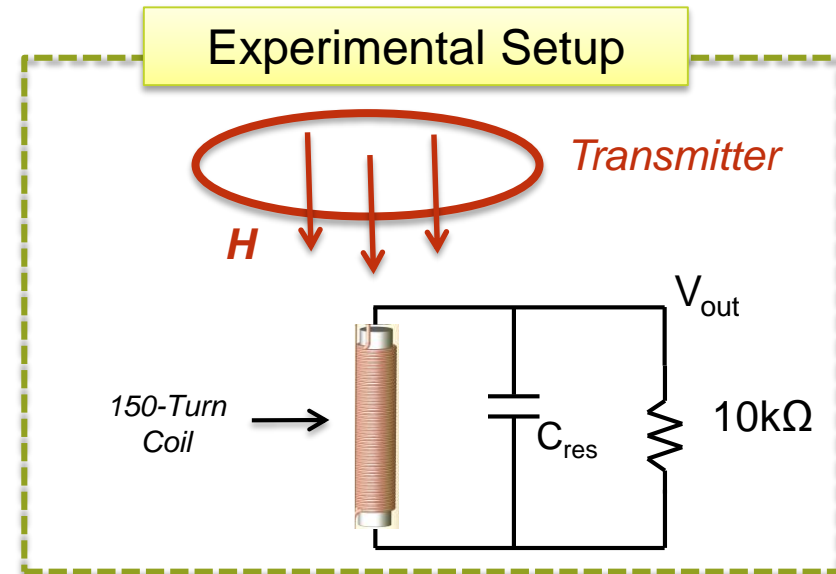


### Prototype with 0201 Caps



# Tuning of the Coils

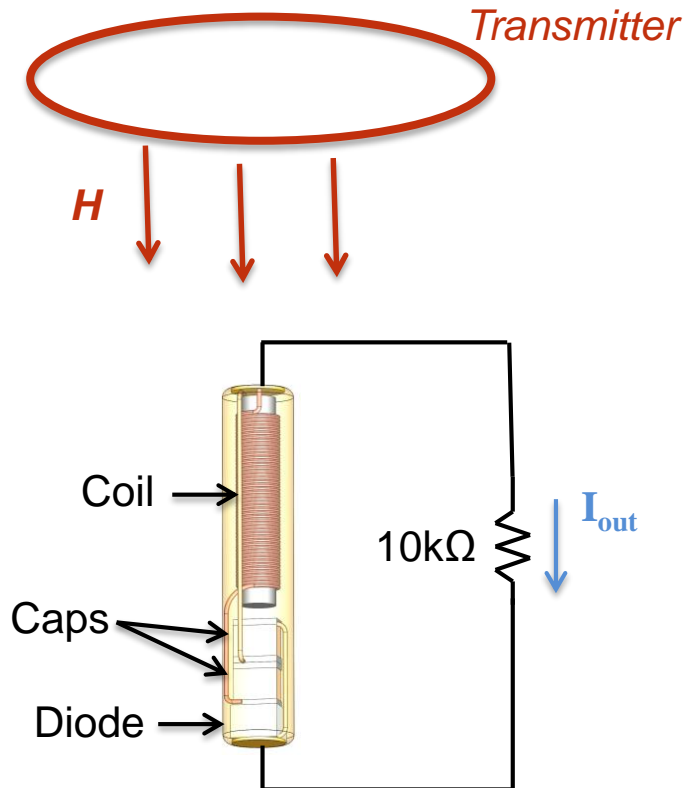
- Coil of  $25\mu\text{H}$  tuned with  $7\text{pF}$  capacitor, resulting in a quality factor of 12
- Approximately ten individually addressable stimulators over  $1 - 20\text{MHz}$



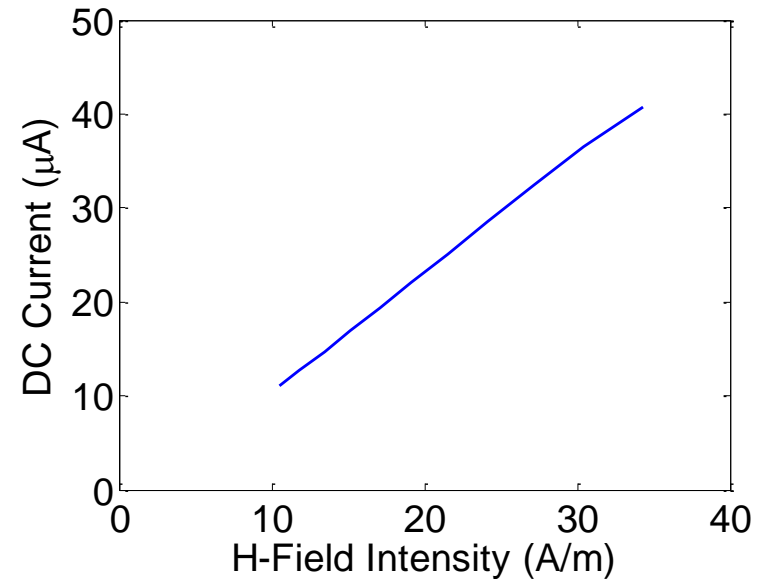
# Measuring DC Output Current of Coils

At maximum allowed magnetic field, the stimulator delivers  $>40\mu\text{A}$  to a  $10\text{k}\Omega$  load

## Experimental Setup

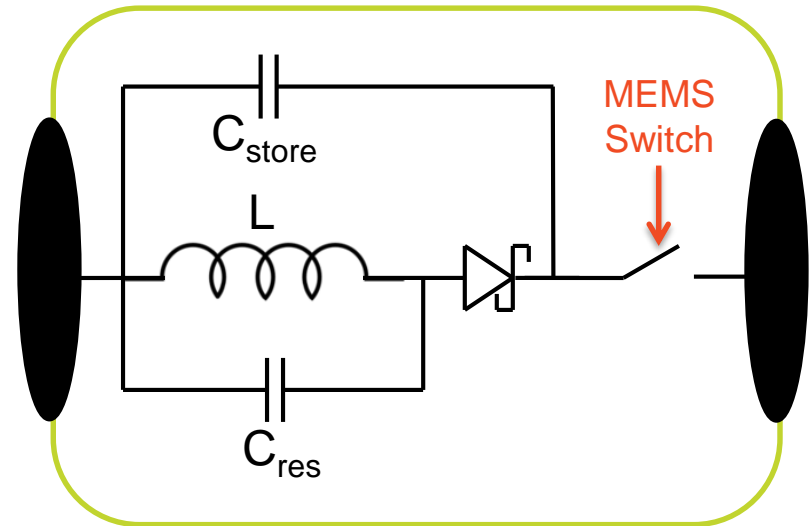
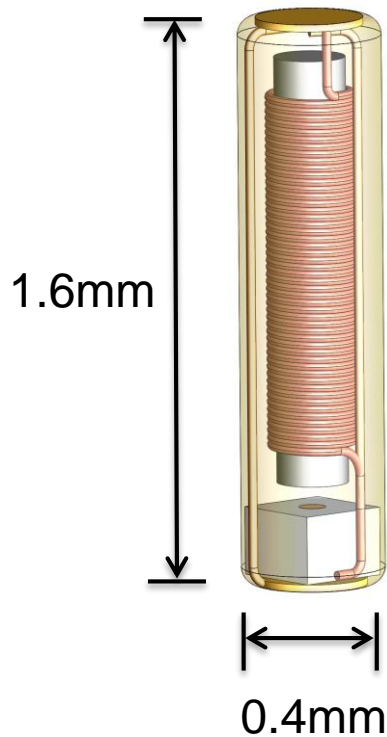


## Output Current vs Applied Field



# Going Forward

- Integration of capacitors into disc electrodes will reduce length to 1.6mm
- Exploring a magnetically actuated MEMS switch to increase Q



# Thank You

---

## Draper Laboratory

- Parshant Kumar
- Jon O'Brien
- Andrew Magyar
- Jon Bernstein
- Caroline Bjune
- Amy Duwel
- Brett Ingersoll
- Reed Irion

## University of Texas at Dallas

- Stuart Cogan
- Mario Romero-Ortega



## Massachusetts General Hospital

- Shelley Fried
- Seungwoo Lee

